

**GAS GENERANTS CONTAINING SILICONE FUELS**  
**CROSS-REFERENCE TO RELATED APPLICATIONS**

This application claims the benefit of U.S. Provisional

5 Application Serial Nos. 60/154,242 and 60/154,293 filed September 16, 1999.

**BACKGROUND OF THE INVENTION**

**Field of the Invention**

The present invention generally relates to gas generant compositions for  
10 inflators of occupant restraint systems. High gas yield gas generants often  
lose large amounts of heat to the inflator body and surroundings during  
combustion, and thereby result in a lower generant burn rate and a reduced  
performance. Compositions provided in accordance with the present invention  
exhibit a rapid and sustained burn at ambient pressure. Other benefits may  
15 include a relatively lower combustion temperature and/or an increase in the  
moles of gas produced per gram of gas generant composition.

Certain applications incorporating gas generation require a relatively fast  
burn at ambient pressure, as compared to known nonazide gas generant  
compositions. Many known nonazide compositions simply cannot sustain a  
20 combustion burn rate, adequate for inflation of an airbag for example, under  
ambient conditions. To overcome this disadvantage, combustion must occur  
in pressurized conditions. As a result, the combustion vessel (an airbag gas  
generator for example) must be manufactured to accommodate pressures of  
25 1000 pounds per square inch (psi) or greater. The need to pressurize the  
combustion vessel during combustion requires a more robust inflator and  
therefore increases the manufacturing costs.

Certain gas generant compositions or propellants containing silicone and  
a perchlorate oxidizer (compositions containing silicone and potassium  
perchlorate, for example) exhibit a relatively rapid burn rate and sustainable  
30 combustion at ambient pressure. Nevertheless, to sustain combustion, the

combustion temperature is quite hot. As a result, these compositions are not suitable for certain applications unless an adequate heat sink is also provided. Therefore, the manufacturing cost of the inflator or combustion vessel again increases.

5       Silicone as a fuel is advantageous over other known nonazide fuels known to be useful in occupant restraint systems, for example. Because silicone does not contain nitrogen, undesirable nitrogen oxides are reduced or eliminated as combustion products. Additionally, silicone also provides elasticity to the gas generant composition thereby reducing the propensity for  
10 fracture of the gas generant over time. Finally, silicone aids in sustaining combustion at ambient pressure.

Therefore, a gas generant composition utilizing silicone as a primary fuel and yet exhibiting a rapid and sustained burn rate along with an acceptable combustion temperature would be an improvement in the art.

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#### SUMMARY OF THE INVENTION

20       The above-referenced problems are resolved by gas generant compositions containing silicone as a fuel; an oxidizer selected from the group including metal and nonmetal perchlorates such as potassium perchlorate, lithium perchlorate, and ammonium perchlorate; and, a coolant selected from the group including metal carbonates, metal bicarbonates, metal oxalates, and metal  
25 hydroxides. In accordance with the present invention, the addition of a coolant to a composition containing a perchlorate oxidizer and a silicone fuel results in a composition that combusts at rapid and sustained burn rates at ambient pressure. Additionally, the combustion temperature is substantially lower than other state of the art compositions.

30       Preferred gas generant compositions contain coolants having more negative heats of formation. Stated another way, preferred coolants of the

present invention will preferably exhibit a relatively greater negative heat of formation. Accordingly, dissociation of the coolant upon combustion of the gas generant composition results in an endothermic combustion reaction thereby resulting in a cooler combustion temperature. Furthermore, when coolants such 5 as strontium carbonate are employed, strontium silicate is formed thereby forming an insulation around the propellant as it burns. As a result, the heat that is released upon combustion is conserved by the insulating effect of the metal silicate. Although strontium carbonate is the most preferred coolant, other metal salts also exhibit similar characteristics.

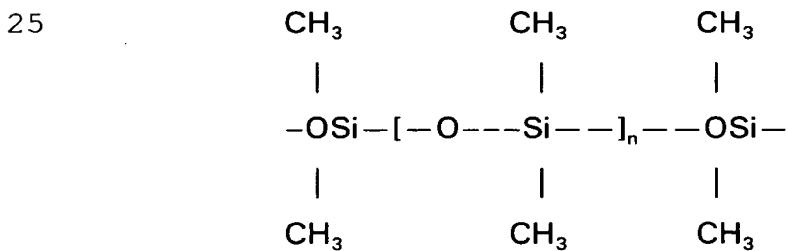
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#### DESCRIPTION OF THE PREFERRED EMBODIMENT(S)

In accordance with the present invention, compositions containing at least one silicone polymer (organosiloxane polymers) as a fuel, at least one oxidizer, and at least one coolant component containing a metallic salt and/or 15 base, combust at ambient pressure at acceptable combustion temperatures.

Silicone is defined as any of a large group of siloxane polymers based on a structure consisting of alternate silicon and oxygen atoms with various organic radicals (or functional groups) attached to the silicon. Radicals include, but are not limited by the group including methyl, methoxy, and amino.

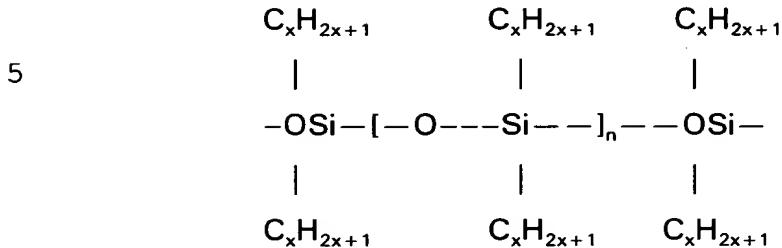
20 The term "silicone" as used herein will be understood in its generic sense. Hawley describes silicone (organosiloxane) as any of a large group of siloxane polymers based on a structure consisting of alternate silicon and oxygen atoms with various organic radicals attached to the silicon:



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*Formula I: Silicone Example*

Or, silicone can be more generically represented as shown in Formula 2:



10 *Formula 2: Silicone Example*

Note, "n" in the Formulas indicates a multiple of the polymeric group or portion of the molecule given within the brackets, to include the organic groups attached to the silicon.

Exemplary silicones include those disclosed in U.S. Patent Nos.

15 5,589,662, 5,610,444, and 5,700,532, and, in TECHNOLOGY OF POLYMER COMPOUNDS AND ENERGETIC MATERIALS, Fraunhofer-Institut fur Chemische Technologie (ICT), 1990, each reference and document herein incorporated by reference.

The compositions of the present invention contain silicone as a fuel. The  
20 fuel component is provided at 10-25% by weight of the gas generant composition.

The gas generant compositions of the present invention contain one or more primary oxidizers selected from the group including metal and  
25 nonmetal perchlorates.

If desired, exemplary secondary oxidizers include but are not limited to phase stabilized ammonium nitrate, ammonium nitrate, potassium nitrate, and strontium nitrate. Stated another way, secondary oxidizers may be selected from the group including metal and nonmetal chlorates, oxides,  
30 nitrates, and nitrites, or other well known oxidizers.

A coolant is selected from the group including metal carbonates,

metal oxalates, metal bicarbonates, and metal hydroxides. "Metal" is defined as alkali, alkaline earth, and transitional metals. Exemplary coolants include but are not limited to strontium carbonate, magnesium carbonate, calcium carbonate, potassium carbonate, strontium oxalate, and magnesium hydroxide.

5 An additional benefit of the coolant is that upon combustion, the resulting metal and silicate ions formed during combustion will form metal silicates. As a result, a coating will form within the combustion chamber and insulate the propellant within the pressure vessel thereby conserving the heat of reaction and contributing to a strong and sustained burn rate at ambient  
10 pressure.

Preferred compositions include silicone, a metal perchlorate oxidizer, and an alkaline earth carbonate. A most preferred composition contains silicone, potassium perchlorate, and strontium carbonate. This composition results in the formation of strontium silicates. The substantial  
15 negative heat of formation of strontium carbonate results in an endothermic combustion reaction. As a result the combustion temperature is reduced. This counters the heat loss that generally results from high gas yield gas generants.

Metal silicates are formed upon combustion of the gas generant compositions containing silicone and metal salts as coolants. Strontium  
20 silicates (or other metal silicates) function as ceramic insulators. Therefore, the metal silicates formed upon combustion insulate the propellant chamber thereby maintaining sufficient heat proximate to the burning surface of the propellant and improving combustion characteristics. As such, the heat of combustion is endothermically minimized by the negative heat of formation of  
25 the coolant, and is then retained during combustion by the additional insulating benefit.

The gas generant composition contains 10-25% by weight of silicone, 30-85% by weight of a primary oxidizer, and 1-30% by weight of a coolant. If desired, one or more secondary oxidizers are employed at 30-50%  
30 by weight of the gas generant composition. The gas generant constituents in similarly sized granular or smaller particulates are added to a tumble blender at

100°C and homogeneously blended, preferably for at least two hours. Silicone is preferably added as a resin that is previously blended with a curing agent. In general, the order in which the constituents are added is not critical so long as they are homogeneously blended. Other known wet and dry blending methods 5 may also be used. Once blending is complete, the gas generant constituents may be extruded or formed into specific shapes such as elongated extrusions, pellets, sheets, or granules.

Table 1 exemplifies the present invention. As shown in the table, compositions consisting of silicone and a perchlorate oxidizer have rapid and 10 sustained burn rates (at 3000 psi) greater than or equal to one inch per second. These combustion properties have been observed at ambient pressure wherein the burn rate is approximately 0.4 inches per second or greater. Nevertheless, the combustion temperatures are relatively high. See Examples 2 and 3. However, when a coolant such as a metal carbonate is added, the temperatures 15 in certain cases are notably reduced. See Examples 17, 21, and 24, for example.

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Example	Formulation	Mol gas/100g	Tc @ 3000psi	Density g/cc	Gas Yield %	Comment
1	82% Sr(NO <sub>3</sub> ) <sub>2</sub> 18% Silicone	1.6	2100	2.20	45.2	Slow ignition and burning; well-formed slag
2	79% KClO <sub>4</sub> 21% Silicone	1.4	3182	1.90	40.8	Rapid and sustained burn at ambient pressure
3	80% KClO <sub>4</sub> 20% Silicone	1.4	3130	1.93	43.4	Rapid and sustained burn at ambient pressure
4	31% KClO <sub>4</sub> 19% Silicone 50% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.5	2100	2.08	43.2	Slower ignition and burning than Ex.2 and 3; well-formed slag
5	30% KClO <sub>4</sub> 20% Silicone 50% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.6	2100	2.05	46.7	Slower ignition and burning than Ex.2 and 3; well-formed slag
6	30% LiClO <sub>4</sub> 22% Silicone 48% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.7	2222	1.98	46.7	Slower ignition and burning than Ex.2 and 3; well-formed slag
7	20% LiClO <sub>4</sub> 20% Silicone 60% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.6	2099	2.07	46.4	Slower ignition and burning than Ex.2 and 3; well-formed slag

Example	Formulation	Mol gas/100g	Tc @ 3000psi	Density g/cc	Gas Yield %	Comment
8	29% LiClO <sub>4</sub> 20% Silicone 40% Sr(NO <sub>3</sub> ) <sub>2</sub> 11% NH <sub>4</sub> NO <sub>3</sub>	1.9	2207	1.93	52.6	Burn is slower than non-AN formulas; higher gas yield
9	45% LiClO <sub>4</sub> 20% Silicone 35% NH <sub>4</sub> NO <sub>3</sub>	2.6	2923	1.70	65.8	Burn is slower than non-AN formulas; higher gas yield
10	27% LiClO <sub>4</sub> 20% Silicone 35% Sr(NO <sub>3</sub> ) <sub>2</sub> 18% NH <sub>4</sub> NO <sub>3</sub>	2.2	2379	1.88	55.9	Burn is slower than non-AN formulas; higher gas yield
11	37% LiClO <sub>4</sub> 19% Silicone 44% NH <sub>4</sub> NO <sub>3</sub>	2.8	2841	1.67	69.8	Burn is slower than non-AN formulas; higher gas yield
12	53% KClO <sub>4</sub> 20% Silicone 27% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.5	2594	2.00	42.0	Slower ignition and burning than Ex.2 and 3; well-formed slag
13	27% LiClO <sub>4</sub> 20% Silicone 36% Sr(NO <sub>3</sub> ) <sub>2</sub> 17% NH <sub>4</sub> NO <sub>3</sub>	2.0	2000	1.93	55.4	Burn is slower than non-AN formulas; higher gas yield but liberates H <sub>2</sub> and CO
15	58% LiClO <sub>4</sub> 20% Silicone 22% Na <sub>2</sub> CO <sub>3</sub>	1.5	3291	1.90	51.0	Rapid and sustained burn at ambient pressure
16	58% LiClO <sub>4</sub> 20% Silicone 22% SrCO <sub>3</sub>	1.5	2296	2.00	47.5	Rapid and sustained burn at ambient pressure
17	58% LiClO <sub>4</sub> 20% Silicone 22% CaCO <sub>3</sub>	1.5	2100	1.95	51.8	Rapid and sustained burn at ambient pressure
18	71% LiClO <sub>4</sub> 19% Silicone 10% C <sub>3</sub> H <sub>6</sub> N <sub>6</sub>	1.9	3161	1.83	56.2	
19	49% KClO <sub>4</sub> 21% Silicone 30% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.5	2633	1.98	41.9	Slower ignition and burning than Ex.2 and 3; well-formed slag
20	20% Silicone 80% NH <sub>4</sub> NO <sub>3</sub>	3.4	3094	1.64	83.8	Burn is slower than non-AN formulas; higher gas yield but liberates H <sub>2</sub> , HCl, CO
21	58% LiClO <sub>4</sub> 20% Silicone 22% CaC <sub>2</sub> O <sub>4</sub>	1.6	2277	1.86	53.7	Rapid and sustained burn at ambient pressure
22	51% LiClO <sub>4</sub> 22% Silicone 27% NH <sub>4</sub> NO <sub>3</sub>	2.4	3007	1.7	61.9	Burn is slower than non-AN formulas; higher gas yield but liberates H <sub>2</sub> and CO
23	10% KClO <sub>4</sub> 20% Silicone 70% Sr(NO <sub>3</sub> ) <sub>2</sub>	1.6	2100	2.11	55.9	Slower ignition and burning than Ex.2 and 3; well-formed slag
24	60% KClO <sub>4</sub> 20% Silicone 20% SrCO <sub>3</sub>	1.5	2363	2.03	37.5	Rapid and sustained burn at ambient pressure

Table 1

In general, compositions containing ammonium nitrate and/or other metal nitrates or secondary oxidizers in amounts greater than 50% by weight of the gas generant composition did not exhibit sufficient burn rates (.4 inches per second or greater) at ambient pressure. Strontium salts that are not oxidizers 5 are preferred given the greater cooling effect. Compare Examples 19 and 24.

Furthermore, in accordance with the present invention, certain compositions exhibit relatively higher temperatures than a preferred embodiment containing silicone, strontium carbonate and potassium perchlorate, for example, but still sustained rapid combustion at ambient pressure. As a result, these 10 compositions are still desirable from the perspective that a less robust inflator is required.

Combustion properties may be tailored by adding known ballistic modifiers and catalysts if desired.

The gas generant constituents of the present invention are 15 available from well-known sources such as Fisher Chemical or Aldrich. The silicone polymers may be purchased, for example, from General Electric in Waterford, New York.

The compositions of the present invention are useful in many applications requiring gas generation. These compositions have particular utility as gas 20 generant compositions that may be combusted to inflate an airbag in a vehicle occupant protection system, for example.

While specific embodiments have been described in detail, those with ordinary skill in the art will appreciate that various modifications and alternatives to those details could be developed in light of the overall teachings 25 of the disclosure. Accordingly, the particular arrangements disclosed are meant to be illustrative only and not limiting as to the scope of the invention, which is to be given the full breadth of any claims which are derivable from the description herein, and any and all equivalents thereof.